## Models & numerical schemes for free surface flows Beyond the Saint-Venant system

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#### NumHyp Roscoff - September 2011

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#### Navier-Stokes vs. Saint-Venant

2D Navier-Stokes 
$$H, \mathbf{u} = (u, w)$$

$$\begin{cases} \operatorname{div} \underline{\mathbf{u}} = \mathbf{0}, \\ \underline{\dot{\mathbf{u}}} + (\underline{\mathbf{u}} \cdot \nabla) \underline{\mathbf{u}} + \nabla p = \mathbf{G} + \operatorname{div} \underline{\underline{\Sigma}}, \end{cases}$$

<u>Saint-Venant</u>  $H, \bar{u}$ 

$$\begin{cases} \frac{\partial H}{\partial t} + \frac{\partial (H\bar{u})}{\partial x} = 0, \\ \frac{\partial (H\bar{u})}{\partial t} + \frac{\partial}{\partial x} (H\bar{u}^2 + \frac{g}{2}H^2) = -gH\frac{\partial z_b}{\partial x} - \kappa(\bar{u}) \end{cases}$$

Advantages of Saint-Venant compared to Navier-Stokes

But more accurate approximation of the Navier-Stokes system are needed

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## Outline & Main ideas

#### Beyond the Saint-Venant system

- Multilayer approximations of the Navier-Stokes system
  - o valid for miscible fluids with variable density
  - with non-hydrostatic terms
- Numerical schemes & simulations
  - $\circ\;$  kinetic description
  - discretization of the source terms
- Hydrodynamics & couplings
  - biological or erosion models

## Beyond the Saint-Venant system



• Many contributions (Audusse, Bouchut, LeVeque, Pares, ...)

 $\Rightarrow$ 

- Valid for non-miscible fluids
- Pb. with underlying physics,...

#### Key idea

Saint-Venant  $u(x, z, t) \approx \overline{u}(x, t)$  Multilayer Saint-Venant  $u(x, z, t) \approx \sum_{\alpha=1}^{N} \mathbf{1}_{z \in L_{\alpha}(x, t)} u_{\alpha}(x, t)$ 

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### Model derivation

# $\frac{\text{Starting point}}{\text{(Euler hydro)}} \left\{ \begin{array}{l} \frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0\\ \frac{\partial u}{\partial t} + \frac{\partial u^2}{\partial x} + \frac{\partial uw}{\partial z} + \frac{\partial p}{\partial x} = 0\\ \frac{\partial p}{\partial z} = -g \end{array} \right.$

#### **Obtained model**

 Weak form (ℙ<sup>t</sup><sub>0</sub>) of the continuity equation with ℙ<sup>t</sup><sub>0</sub> = {1<sub>z∈L<sub>α</sub>(x,t)</sub>, 1 ≤ α ≤ N}

$$\frac{\partial h_{\alpha}}{\partial t} + \frac{\partial h_{\alpha} u_{\alpha}}{\partial x} = G_{\alpha+1/2} - G_{\alpha-1/2}$$

 $\begin{array}{ll} G_{\alpha+1/2} &= \frac{\partial z_{\alpha+1/2}}{\partial t} + u_{\alpha+1/2} \frac{\partial z_{\alpha+1/2}}{\partial x} - w_{\alpha+1/2} = \sum_{j=1}^{\alpha} \frac{\partial h_j}{\partial t} + \frac{\partial h_j u_j}{\partial x} \\ G_{1/2} &= G_{N+1/2} = 0 \text{ (kinematic boundary conditions)} \end{array}$ 

## Model derivation

# $\frac{\text{Starting point}}{\text{(Euler hydro)}} \left\{ \begin{array}{l} \frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0\\ \frac{\partial u}{\partial t} + \frac{\partial u^2}{\partial x} + \frac{\partial uw}{\partial z} + \frac{\partial p}{\partial x} = 0\\ \frac{\partial p}{\partial z} = -g \end{array} \right.$

#### **Obtained model**

• Weak form  $(\mathbb{P}_0^t)$  of the Euler system  $\mathbb{P}_0^t = \{\mathbf{1}_{z \in L_\alpha(x,t)}, \ 1 \le \alpha \le N\}$ 

$$\begin{cases} \frac{\partial H}{\partial t} + \sum_{\alpha=1}^{N} \frac{\partial}{\partial x} (h_{\alpha} u_{\alpha}) = 0\\ \frac{\partial (h_{\alpha} u_{\alpha})}{\partial t} + \frac{\partial}{\partial x} (h_{\alpha} u_{\alpha}^{2} + \frac{g}{2} h_{\alpha} f(\{h_{j}\}_{j \ge \alpha})) = F_{\alpha+1/2} - F_{\alpha-1/2}\\ \frac{\partial E_{\alpha}}{\partial t} + \frac{\partial}{\partial x} (u_{\alpha} (E_{\alpha} + \frac{g}{2} h_{\alpha} H)) = E_{\alpha+1/2} - E_{\alpha-1/2} \end{cases}$$

- Only one ''global'' continuity equation,  $\mathit{H} = \sum \mathit{h}_{lpha}$
- Exchange terms  $G_{\alpha+1/2}$ ,  $F_{\alpha+1/2} = u_{\alpha+1/2}G_{\alpha+1/2} + P_{\alpha+1/2}$ ,  $E_{\alpha+1/2} = \frac{u_{\alpha+1/2}^2}{2}G_{\alpha+1/2} + u_{\alpha+1/2}P_{\alpha+1/2}$
- If  $G_{\alpha+1/2} \equiv 0$  non-miscible fluids, N cont. equations

#### Hydrostatic Euler (NS) with varying density (Aud., Brist., Pela., JSM JCP 2010)

#### Starting point

$$\begin{cases} \dot{\rho} + \operatorname{div} (\rho \underline{\mathbf{u}}) = \mathbf{0}, \\ \frac{\dot{\rho} \underline{\mathbf{u}}}{\rho} + (\underline{\mathbf{u}} \cdot \nabla) (\rho \underline{\mathbf{u}}) + \nabla \boldsymbol{p} = \rho \mathbf{G}, \\ \frac{\dot{\rho} \overline{T}}{\rho} + \operatorname{div} (\rho T \underline{\mathbf{u}}) = \mu_T \Delta T, \end{cases}$$

with  $\rho = \rho(\{T, S\}) \quad (= \rho(T, S, H))$ 



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**Obtained model** 

 $u(x,z,t)\approx\sum_{\alpha=1}^{N}\mathbf{1}_{z\in L_{\alpha}}u_{\alpha}(x,t)$ 

$$\begin{cases} \frac{\partial}{\partial t} \sum_{\alpha=1}^{N} (\rho_{\alpha} h_{\alpha}) + \sum_{\alpha=1}^{N} \frac{\partial}{\partial x} (\rho_{\alpha} h_{\alpha} u_{\alpha}) = 0, \\ \frac{\partial (\rho_{\alpha} h_{\alpha} u_{\alpha})}{\partial t} + \frac{\partial}{\partial x} (\rho_{\alpha} h_{\alpha} u_{\alpha}^{2} + \frac{g}{2} h_{\alpha} f(\{\rho_{j} h_{j}\}_{j \ge \alpha})) = \\ + u_{\alpha+1/2} G_{\alpha+1/2} - u_{\alpha-1/2} G_{\alpha-1/2} + Sc. \text{ Terms}, \\ \frac{\partial (\rho_{\alpha} h_{\alpha} T_{\alpha})}{\partial t} + \frac{\partial}{\partial x} (\rho_{\alpha} h_{\alpha} u_{\alpha} T_{\alpha}) = T_{\alpha+1/2} G_{\alpha+1/2} - T_{\alpha-1/2} G_{\alpha-1/2}, \end{cases}$$

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## Properties of the model

• Hyperbolicity ?

quasi-linear form 
$$X = (H, u_1, \dots, u_N, E_1, \dots, E_N)^T$$

$$M(X)\dot{X} + F(X)\frac{\partial X}{\partial x} = 0$$

- "often" hyperbolic
- strictly hyperbolic for N = 2
- o for N > 2, "arrow matrices" and interlacing of eigenvalues

$$rac{1}{N}\sum_{1}^{N}u_{i}^{2}\leq gH$$
 (generalized Froude number)

- o family of entropies
- When  $N \to \infty$  ?

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### Non-hydrostatic terms

#### The Euler system

$$\begin{cases} \frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0\\ \frac{\partial u}{\partial t} + \frac{\partial u^2}{\partial x} + \frac{\partial uw}{\partial z} + \frac{\partial p}{\partial x} = 0\\ \frac{\partial w}{\partial t} + \frac{\partial uw}{\partial x} + \frac{\partial w^2}{\partial z} + \frac{\partial p}{\partial z} = -g \end{cases}$$

#### Two main approaches

- Irrotational flows
  - many contributors (Bona, Dutyk, Lannes, Saut,...)
- Non-hydrostatic Saint-Venant system
  - mainly  $\frac{\partial w}{\partial t}$  (Peregrine,...)
  - for shallow water flows

## Approximation of the Euler (NS) system

#### (JSM M3AS'11)

#### Starting point

$$(S) \begin{cases} \frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0\\ \frac{\partial u}{\partial t} + \frac{\partial u^2}{\partial x} + \frac{\partial uw}{\partial z} + \frac{\partial p}{\partial x} = 0\\ \frac{\partial w}{\partial t} + \frac{\partial uw}{\partial x} + \frac{\partial w^2}{\partial z} + \frac{\partial p}{\partial z} = -g \end{cases}$$

- For Shallow Water systems : simple vertical mean
- Key Idea : vertical momenta  $\int_{z_b}^{\eta} z^i (S) dz$ , i = 0, 1
- Compact form

$$\frac{\partial X}{\partial t} + \frac{\partial}{\partial x} F(X, \bar{p}) - R(X, \bar{p}) = S(X, \bar{p})$$
  
with  $X = (H, \bar{u}, \bar{w}, \ldots)$ 

Possibly vertical semi-discretization (multilayer)

$$u(x,z,t) \approx \sum_{\alpha=1}^{N} \mathbf{1}_{z \in L_{\alpha}}(z) u_{\alpha}(x,t)$$

## Averaged Euler system (non-hydrostatic Saint-Venant)

$$\begin{split} &\frac{\partial H}{\partial t} + \frac{\partial}{\partial x} (H\overline{u}) = 0\\ &\frac{\partial}{\partial t} \left( \frac{\eta^2 - z_b^2}{2} \right) + \frac{\partial}{\partial x} \left( \frac{\eta^2 - z_b^2}{2} \overline{u} \right) - H\overline{w} = 0\\ &\frac{\partial}{\partial t} (H\overline{u}) + \frac{\partial}{\partial x} (H\overline{u}^2 + H\overline{p}) = -p_b \frac{\partial z_b}{\partial x}\\ &\frac{\partial}{\partial t} \left( \frac{\eta^2 - z_b^2}{2} \overline{u} \right) + \frac{\partial}{\partial x} \left( \frac{\eta^2 - z_b^2}{2} \overline{u}^2 + \int_{z_b}^{\eta} zp \ dz \right) - H\overline{w} \ \overline{u} = -\frac{1}{2} \frac{\partial z_b^2}{\partial x} p_b\\ &\frac{\partial}{\partial t} (H\overline{w}) + \frac{\partial}{\partial x} (H\overline{wu}) = p_b - gH\\ &\frac{\partial}{\partial t} \int_{z_b}^{\eta} z\hat{w} \ dz + \frac{\partial}{\partial x} \overline{u} \int_{z_b}^{\eta} z\hat{w} \ dz - \int_{z_b}^{\eta} \hat{w}^2 \ dz - H\overline{p} = z_b p_b - g \frac{\eta^2 - z_b^2}{2} \end{split}$$

• Only 5 unknowns  $H, \overline{u}, \overline{w}, \overline{p}, p_b...$  but only 5 independant equations

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## What to do with such models ?

- A family of models approximating the Navier-Stokes system
  - only formal convergence as  $N o \infty$
  - $\circ\,$  math. analysis ?
- Good candidates
  - rigourous derivation process
  - energy balance, entropies
- Simpler than the corresponding Navier-Stokes system
  - independant of z, fixed meshes
- But not so simple to analyse & discretize !

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## Kinetic approach for conservation laws

- A fantastic tool for
  - physical understanding (upwinding)
  - mathematical analysis
  - numerical analysis and schemes
- Basis : adopt a microscopic description (Boltzmann)

Cont. model 
$$\Leftrightarrow \frac{\partial M}{\partial t} + \xi \frac{\partial M}{\partial x} - g \frac{\partial z_b}{\partial x} \frac{\partial M}{\partial \xi} = Q(x, t, \xi)$$

- $M(x, t, \xi)$  particle density,  $Q(x, t, \xi)$  collision term (= 0 a.e.)
- $\int_{\mathbb{R}} \xi^{p} M d\xi$  gives the macroscopic variables
- linear transport equation + Vlasov
- Only kinetic representations and not kinetic formulations

#### Kinetic representation of the Saint-Venant system

• Gibbs equilibrium  $M(x, t, \xi) = \frac{H}{c}\chi\left(\frac{\xi-\bar{u}}{c}\right)$  with  $c = \sqrt{gH/2}$ where  $\chi(\omega) = \chi(-\omega) \ge 0$ ,  $\operatorname{supp}(\chi) \subset \Omega$ ,  $\int_{\mathbb{R}}\chi(\omega) = \int_{\mathbb{R}}\omega^{2}\chi(\omega) = 1$ 

#### Proposition (Audusse, Bristeau, Perthame)

The functions  $(H, \bar{u}, E)(t, x)$  are strong solutions of the Saint-Venant system if and only if  $M(x, t, \xi)$  is solution of the kinetic equation

$$(\mathcal{B}), \qquad \frac{\partial M}{\partial t} + \xi \frac{\partial M}{\partial x} - g \frac{\partial z_b}{\partial x} \frac{\partial M}{\partial \xi} = Q(x, t, \xi)$$

where  $Q(t, x, \xi)$  is a "collision term".

- Macroscopic variables  $(H, \bar{u}, E) = \int_{\mathbb{R}} (1, \xi, \xi^2/2) M \ d\xi$
- A linear transport equation ... easy to upwind

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## Kinetic interpretation for the multilayer system (hydrostatic)

• Gibbs equilibria

• 
$$M_{\alpha}(x, t, \xi) = \frac{h_{\alpha}}{c_{\alpha}} \chi\left(\frac{\xi - u_{\alpha}}{c_{\alpha}}\right)$$
, with  $c_{\alpha} = \sqrt{gf(\{h_j\}_{j \ge \alpha})}$   
•  $N_{\alpha+1/2}(x, t, \xi) = G_{\alpha+1/2} \delta\left(\xi - u_{\alpha+1/2}\right)$ ,

Proposition (Audusse, Bristeau, Perthame, JSM 2009) The functions  $(h_{\alpha}, u_{\alpha}, E_{\alpha})(t, x)$  are strong solutions of the multilayer Saint-Venant system if and only if the set  $\{M_j(x, t, \xi)\}_{j=1}^N$  is solution of the kinetic equations

$$\frac{\partial M_{\alpha}}{\partial t} + \xi \frac{\partial M_{\alpha}}{\partial x} - N_{\alpha+1/2} + N_{\alpha-1/2} = Q_{\alpha}(x, t, \xi)$$

- source terms (exchanges, pressure)
- also for variable density case

#### Kinetic interpretation for the Euler system (JSM, M3AS'11)

- Starting point (Euler)  $\begin{cases} \frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0\\ \frac{\partial u}{\partial t} + \frac{\partial u^2}{\partial x} + \frac{\partial uw}{\partial z} + \frac{\partial p}{\partial x} = 0\\ \frac{\partial w}{\partial t} + \frac{\partial uw}{\partial x} + \frac{\partial w^2}{\partial z} + \frac{\partial p}{\partial z} = -g \end{cases}$
- Kinetic interpretation for the averaged Euler system

$$(B_M) \quad \frac{\partial M}{\partial t} + \xi \frac{\partial M}{\partial x} - g \frac{\partial M}{\partial \gamma} = Q_1,$$
  
$$(B_{R,M}) \quad \frac{\partial R}{\partial t} + \xi \frac{\partial R}{\partial x} - \gamma M = Q_2,$$

with the Gibbs equilibria

$$M(x, t, \xi, \gamma) = \frac{H}{c_1 c_2} \chi\left(\frac{\xi - \overline{u}}{c_1}\right) \psi\left(\frac{\gamma - \overline{w}}{c_2}\right)$$
$$R(x, t, \xi, \gamma) = \frac{\eta^2 - z_b^2}{2c_3} \chi\left(\frac{\xi - \overline{u}}{c_3}\right) \delta\left(\gamma - \breve{w}\right)$$

• Proof:  $\int_{\mathbb{R}^2} (1,\xi,\gamma,|\xi|^2/2) \mathcal{B}_M d\xi d\gamma$ ,  $\int_{\mathbb{R}^2} (1,\xi,\gamma) \mathcal{B}_{R,M} d\xi d\gamma$ 

Also multilayer approximation

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Main properties of the schemes (hydrostatic models)

• 
$$f_i^{n+1}(\xi) = M_i^n(\xi) - \xi \sigma_i^n \left( M_{i+1/2}^n(\xi) - M_{i-1/2}^n(\xi) \right) + \Delta t^n S_i^n(\xi)$$

- Positive schemes (CFL=1 but more complex)
- 2<sup>nd</sup> order schemes (space & time)
- Maximum principle (tracer)
- Well balanced (with hydrostatic reconstruction)
- The source terms (pressure)

$$gH\frac{\partial z_b}{\partial x} \Rightarrow g\frac{\partial z_b}{\partial x}\frac{\partial M}{\partial \xi}, \quad \frac{\partial z_{\alpha+1/2}}{\partial x}\frac{\partial M_{\alpha}}{\partial \xi}$$

• kinetic interpretation useful for discretization

• Numerical cost  $N \times SW$ , possibly mesh adaptation

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#### Analytical validation (I) (Boulanger, JSM 2011)

- Analytical solutions to the Euler system
  - 2D and 3D solutions, for any bottom topography  $z_b(x, y)$
  - with entropic shocks
  - not necessarily free surface flows
  - In 2D (continuous solutions), u and H characterized by

$$u = \alpha \beta \frac{\cos \beta (z - z_b)}{\sin \beta H}, \quad \left(g(H + z_b) + \frac{\alpha^2 \beta^2}{2 \sin(\beta H)^2}\right)_x = 0$$

Recovered by the 2D and 3D codes



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## Analytical validation (II)

• With shocks



• Also without free surface

#### Seism in Japan, march 2011



source IPGP (A. Mangeney)

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seism

## "Validation" with DART buoys





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Hydrodynamics & couplings

#### The next tsunami : Roscoff 6.0 !





## Archimedes law

• Well-balanced schemes

• Stability 
$$\frac{\partial}{\partial x} \left( \int_{z}^{\eta} \rho g \, dz \right) = 0 \qquad \neq \quad \frac{\partial \eta}{\partial x} = 0$$





## Archimedes law (with C. Pares)

• Experimental set up (simulation)



• Velocity field (6 s)



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## Hydrodynamics-biology coupling

Description : algae pool driven into motion by a paddle wheel



Goal : optimize the biomass production by playing on the nutrients supply, water depth, agitation,...

## The biological model

• Droop model (Droop 1983)

$$\begin{cases} \frac{dC_1}{dt} = \mu(\frac{C_2}{C_1}, I)C_1 - RC_1\\ \frac{dC_2}{dt} = -\lambda(C_3, \frac{C_2}{C_1})C_1\\ \frac{dC_3}{dt} = \lambda(C_3, \frac{C_2}{C_1})C_1 - RC_2 \end{cases}$$

- with  $C_1$ : phytoplanktonic carbon,  $C_2$  residual nitrates and  $C_3$  phytoplanktonic nitrogen, I light, R death rate
- Advection, reaction and diffusion PDE's

$$\frac{\partial X}{\partial t} + \nabla . (\mathbf{u}X) = F(X) + \nu \Delta X$$

with  $X = (C_1, C_2, C_3)^T$ 

- Hydrodynamics (u) governed by the Navier-Stokes Eqs
- Multilayer discretization & kinetic interpretation

#### Numerical validation (Boulanger, JSM 2011)

• Analytical solution

(Euler hydro + bio)

$$\begin{cases} \frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0\\ \frac{\partial u}{\partial t} + \frac{\partial u^2}{\partial x} + \frac{\partial uw}{\partial z} + \frac{\partial p}{\partial x} = 0\\ \frac{\partial p}{\partial z} = -g\\ \frac{\partial T}{\partial t} + \frac{\partial uT}{\partial x} + \frac{\partial wT}{\partial z} = f(x, z)T \end{cases}$$



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Models

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#### Raceway



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#### Simulations results



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#### Lagrangian trajectories

• 
$$\frac{dM(t)}{dt} = \mathbf{u}(M(t), t)$$



Poisition of a particle along time and free surface

3d animation

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## For the future

- Numerical analysis & schemes
  - for the full NS system
  - hyperbolicity, entropies,...
  - stability of the schemes
  - towards industrial codes
- Non-hydrostatic models
  - efficient schemes
- Hydrodynamics and couplings
  - o erosion, carriage and associated problems
  - o hydrodynamics-biology coupling, water quality management
- $\Rightarrow$  Control, stabilization, data assimilation,...
  - o everything is more simple at the kinetic level